



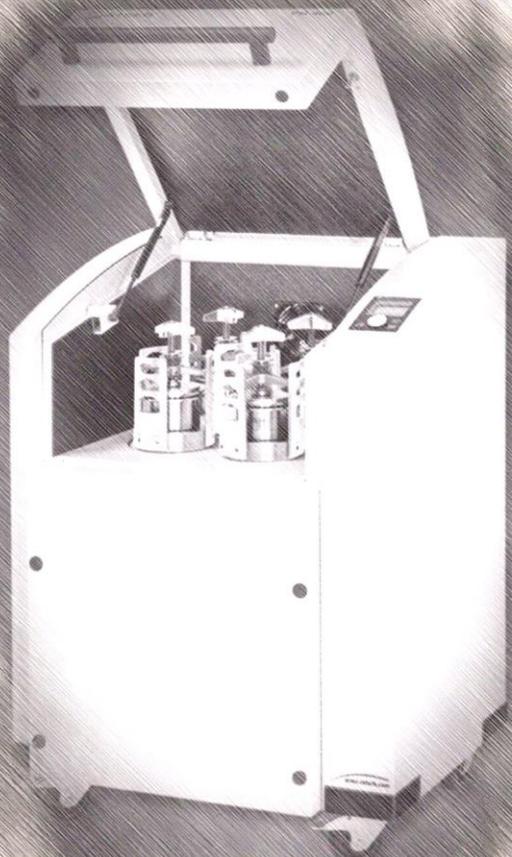
Patricia



Guillermo

" In memoriam "

# SQUID



*Aleado Mecánico*

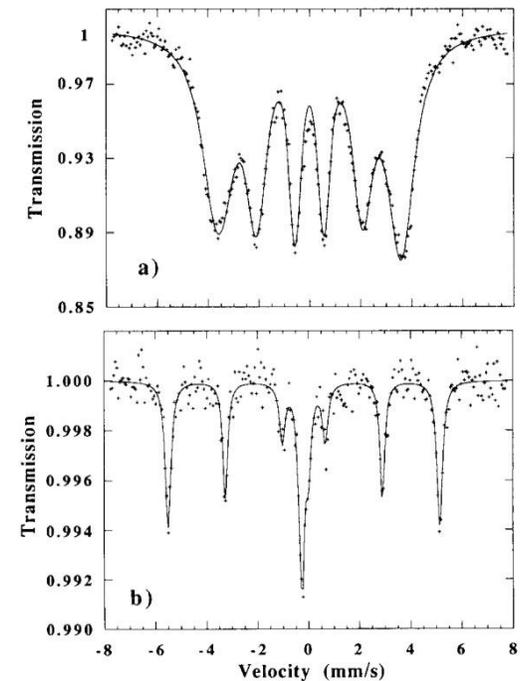
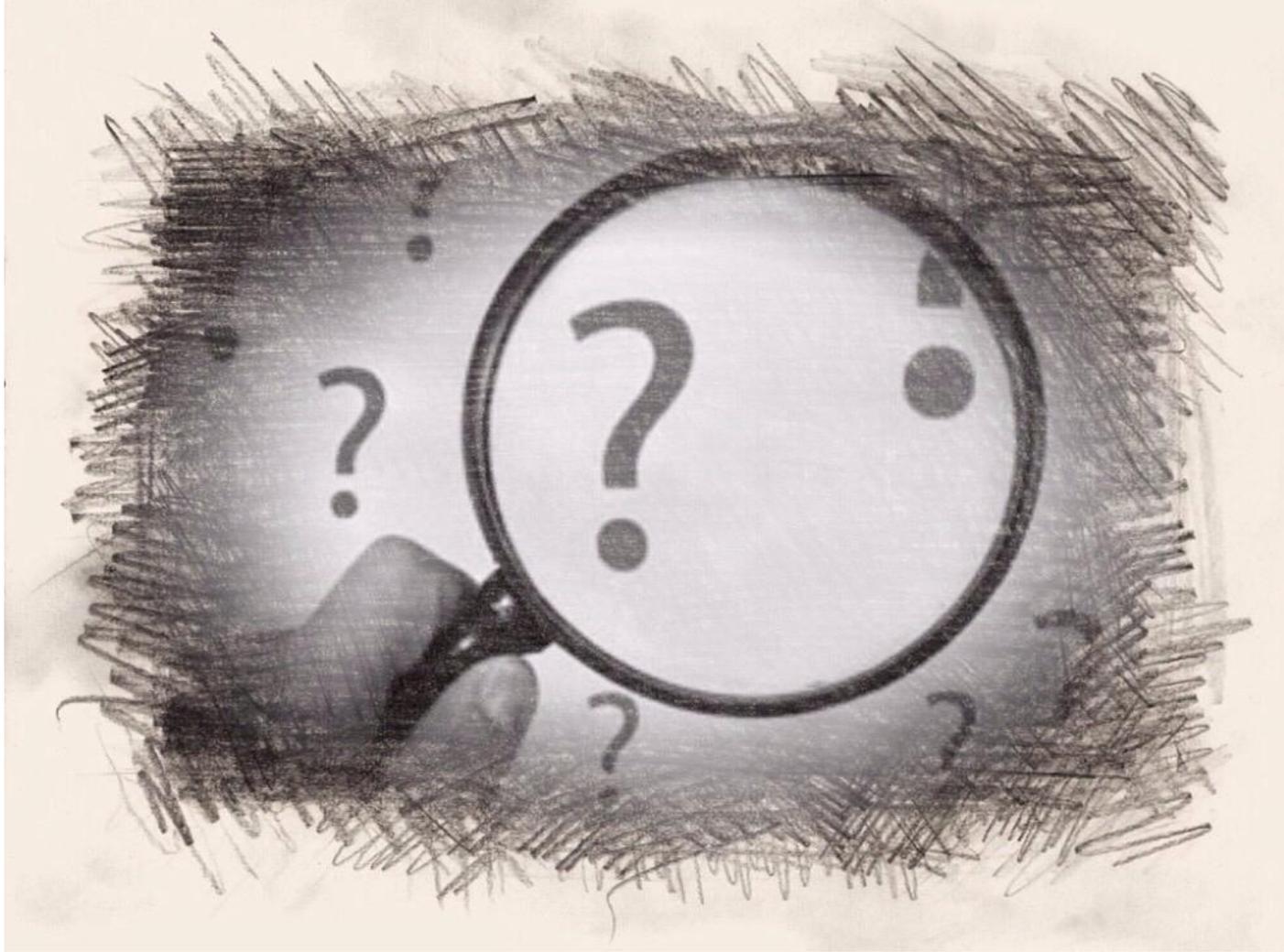


Fig. 3. Room temperature Mössbauer spectra for (a) as-milled and (b) annealed samples. The spectrum in (a) shows a broad distribution of hyperfine fields centered at 21 T and an isomer shift of +0.1  $\text{mms}^{-1}$  relative to  $\alpha$ -Fe at room temperature. The shoulder in the central peak in spectrum (b) shows the existence of a number of paramagnetic Fe atoms in the neighborhood of Cu atoms (see the text).

*Mossbauer*



***Ferromagnetismo***

***¿ Dónde estás?***



*Fe*

+



*Cu*



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Crespo del Arco, Patricia

**Título**

**Propiedades magnéticas de aleaciones nanocristalinas de Fe-Cu. / Patricia Crespo del Arco ; [director] Antonio Hernando Grande**

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Universidad Complutense de Madrid. Facultad de Ciencias Físicas. Departamento de Física de Materiales. Tesis inéditas

### Letter to the Editor

## Magnetic properties of mechanically alloyed Fe–Cu

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Received 25 September 1992; in revised form 22 February 1993

Magnetic properties of equiatomic FeCu alloys, obtained by mechanical alloying, were measured in a temperature range between 5 and 300 K. The as-milled sample consists of a metastable fcc FeCu phase with a temperature dependence of magnetization which follows a  $T^{3/2}$  law. This metastable phase decomposes into Cu and Fe phases with annealing. After annealing at 820 K, the magnetization value at low temperature is 30% smaller than the unannealed state. The Mössbauer spectrum obtained at room temperature shows a paramagnetic Fe phase with a relative resonant area of 30%. These results suggest that after this annealing process 30% of the iron is not in the ferromagnetic  $\alpha$  phase but in a non-magnetic state (with vanishing atomic magnetic moment) or probably forming an antiferromagnetic  $\gamma$ -Fe phase (which is paramagnetic at room temperature).

### 1. Introduction

It has been shown that a metastable fcc FeCu phase can be formed by mechanical alloying. After subsequent annealing a precipitation of bcc iron nanocrystals in the Cu rich fcc matrix has been observed by X-ray diffraction techniques [1]. Magnetic properties of solid solutions of Fe–Cu formed by sputtering have been studied previously [2,3].

The work by Yavari et al. [1] shows an equality of the magnetic moment at room temperature for both the as-milled sample and that annealed at

950 K. By considering the difference in Curie temperatures corresponding to the fcc FeCu phase, 500 K, and that of  $\alpha$  iron, 1000 K, such reported magnetic moments equality at 300 K suggested to us the existence of crossover in the magnetization curves at lower temperatures. Therefore, in order to analyze a possible leakage of iron magnetic moment at intermediate states of the fcc FeCu decomposition process, we have performed a study of the magnetization behavior at low temperature.

### 2. Experimental techniques

Samples were prepared by ball milling as described in ref. [1]. SQUID magnetometry,

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Mössbauer spectroscopy, DSC, EDX analysis, thermogravimetry and X-ray diffraction techniques were applied to as-milled and annealed samples at 820 K. Measurements were carried out from 5 to 300 K. As far as we know this range of temperatures has not been studied before in granular magnetic systems by mechanical alloying.

### 3. Results

Samples with composition  $\text{Fe}_{52.1}\text{Cu}_{47.9}$  (at%), according to EDX analysis, exhibit in the as-milled state a nanocrystalline single fcc phase. The variation of the magnetization with the temperature follows a perfect  $T^{3/2}$  Bloch law up to 200 K (fig. 1), with an exchange stiffness constant of  $96.9 \text{ meV}\text{\AA}^2$ . This is roughly three times smaller than that of pure Fe [4]. The hysteresis loops obtained at 20 and 300 K are shown in fig. 2. The average susceptibility does not change in the temperature range from 20 to 300 K, indicating that the fraction of nanocrystals exhibiting superparamagnetic behavior is negligible. The small hysteresis, with remanent value below 0.01 times the saturation magnetization and coercive field of 40 Oe, shows a negligible structural anisotropy. The lack of structural anisotropy might be a consequence of the disordered distributions of Fe and

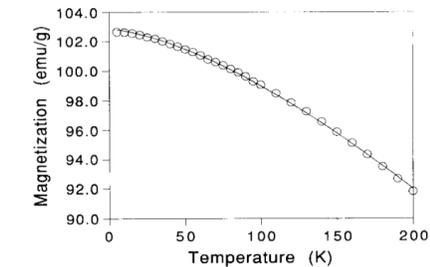


Fig. 1. Temperature dependence of the magnetization for an as-milled sample under an applied field of 5 T. The open circles are the experimental data and the solid line is the fitting according to a  $T^{3/2}$  law.

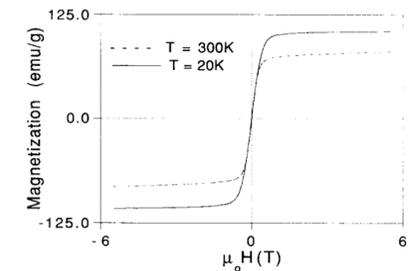


Fig. 2. Hysteresis loops corresponding to the as-milled sample at 20 and 300 K.

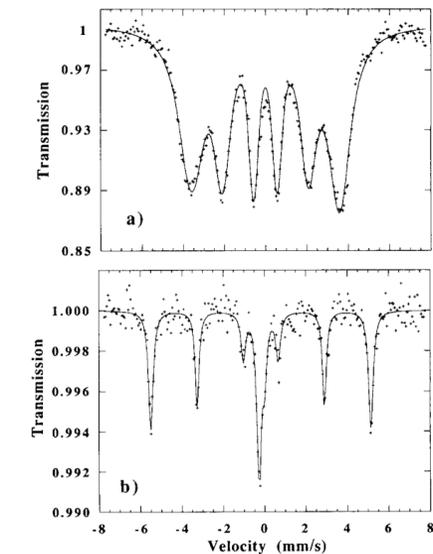


Fig. 3. Room temperature Mössbauer spectra for (a) as-milled and (b) annealed samples. The spectrum in (a) shows a broad distribution of hyperfine fields centered at 21 T and an isomer shift of  $+0.1 \text{ mms}^{-1}$  relative to  $\alpha$ -Fe at room temperature. The shoulder in the central peak in spectrum (b) shows the existence of a number of paramagnetic Fe atoms in the neighborhood of Cu atoms (see the text).

Cu atoms in the fcc structure. The Mössbauer spectrum is shown in fig. 3(a).

The as-milled sample was heated up to 820 K by DSC and its transformation monitored. The choice of the temperature and the heating rate was done on the basis of the work of Yavari [1]. 820 K lies above the peak of the exothermic reaction (which corresponds to the spinodal decomposition of the metastable solid solution) but below the total phase separation and thus we monitor an intermediate state of the Fe segregation. Thermogravimetry showed that oxidation was lower than 1% (the weight increased 0.8% during annealing). After the annealing, which causes the partial dissociation of the metastable fcc FeCu phase into Fe and Cu phases, the X-ray diffraction pattern showed the appearance of bcc Fe. Other new phases were not detected.

As shown in the curves of fig. 4 the magnetization at low temperatures is 30% smaller than the as-milled sample for the same applied field, 5 T. The Mössbauer spectrum, illustrated in fig. 3(b) and obtained at room temperature, shows a perfect pattern of crystalline bcc Fe, with a hyperfine field of 33 T, and a non-ferromagnetic phase which corresponds to 30 at% paramagnetic iron. Nevertheless, no paramagnetic behavior is observed in the low temperature  $M$  vs  $T$  curve. Furthermore, the paramagnetic peak exhibited by the Mössbauer spectrum is compatible with the corresponding  $\gamma$ -Fe analysis of Macedo and Keune. Here Fe atoms with a certain number of

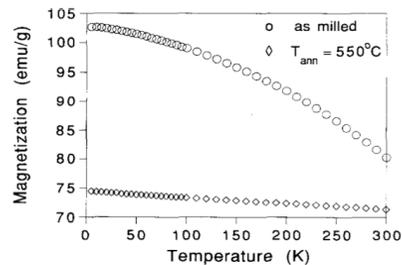


Fig. 4. Temperature dependence of the magnetization for an annealed sample under an applied field of 5 T. The curve of the as-milled sample is also shown.

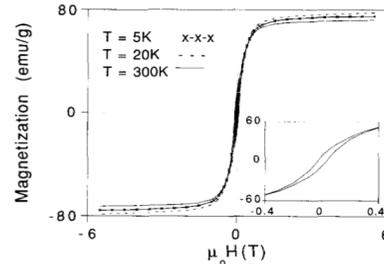


Fig. 5. Hysteresis loops for the annealed sample at 5, 20 and 300 K. The inset (in the same units) shows that the coercive field at 300 K reaches a value of 300 Oe.

Cu neighboring atoms give rise to a less intense quadrupole-splitting [5]. Since the number of Fe atoms does not change with the annealing treatment (at least not higher than 1%) and 30% behave paramagnetically at room temperature, it is reasonable to assume that these paramagnetic atoms are responsible for the 30% reduction of the saturation magnetization observed at low temperatures. However, there is no paramagnetic contribution at low temperature, and therefore we propose they are non-magnetic (with zero atomic moment) or antiferromagnetic in this low temperature range. Both observations, as well as the shape of the corresponding hysteresis loops shown in fig. 5, suggest that two types of Fe clusters have precipitated during annealing: (1)  $\alpha$ -Fe, bcc, which is ferromagnetic and exhibits a coercive force of about 300 Oe at 300 K (fig. 5); and (2) either non-magnetic iron or  $\gamma$ -Fe, fcc, which is antiferromagnetic, with a transition temperature  $T_N$  ranging from 0 to 70 K according to the cluster size [6].

Since the average slope of the magnetization curve does not depend on temperature, we assume that the number of supermagnetic clusters in the range of measuring temperatures is negligible.

The absence of other crystalline phases in X-ray diffraction, the Mössbauer spectra and the reported appearance of  $\gamma$ -Fe in other Fe-Cu alloys obtained by sputtering or other techniques suggest the idea of a 30%  $\gamma$ -Fe segregation, as it

seems likely that Fe clusters with small size retain the fcc Cu phase. (We note that the lattice parameters of Cu ( $a = 3.616 \text{ \AA}$ ) and  $\gamma$ -Fe ( $a = 3.666 \text{ \AA}$ ) are similar and lead to coincidence of the X-ray diffraction peaks.)

The existence of isolated, paramagnetic or non-magnetic Fe atoms in a fcc Cu matrix can not be ruled out but it is difficult to account for 30% of the Fe atoms in this situation, as  $\text{Fe}_{30}\text{Cu}_{70}$  is still a studied alloy [3] and shows no moment reduction for the Fe atoms.

#### 4. Conclusions

The magnetic behavior of nearly equiatomic Fe-Cu alloy obtained by mechanical alloying has been studied at low temperatures for the first time. Similar magnetic measurements carried out on annealed samples have shown that the partial decomposition of the solid solution leads to a decrease of the magnetization at low temperatures. The lack of paramagnetic behavior in the low temperature range as well as the presence of a paramagnetic peak in the Mössbauer spectrum at room temperature suggest the formation of

30%  $\gamma$ -Fe. However, the quenching of the atomic magnetic moment of highly diluted iron atoms is a possibility which cannot be completely disregarded.

#### Acknowledgements

The authors are indebted to Prof. A.E. Berkowitz for helpful comments and to Dr. H.T. Savage for careful reading of the manuscript.

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### CONTRAST MODULATION DURING DECOMPOSITION OF SUPERSATURATED fcc Fe-Cu SOLID AND LIQUID SOLUTIONS.

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**Keywords:** Fe-Cu solutions, spinodal decomposition

**Abstract:** Clear microstructural evidence is obtained from transmission electron microscopy of the occurrence of a modulated structure, as occurring in spinodal decomposition, during the decomposition of metastable mechanically alloyed Fe<sub>50</sub>Cu<sub>50</sub> solid solutions and liquid quenched (Fe<sub>20</sub>Cu<sub>80</sub>)<sub>99</sub>B<sub>1</sub>.

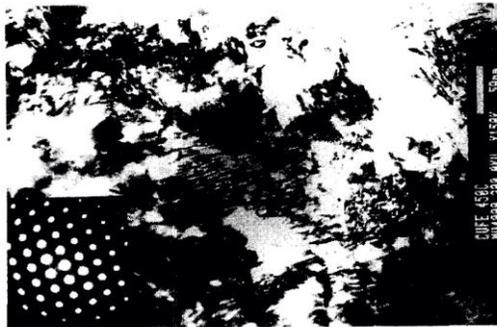


Figure 1.- TEM bright field image of Fe<sub>50</sub>Cu<sub>50</sub> mechanically alloyed and heated up to 723 K.

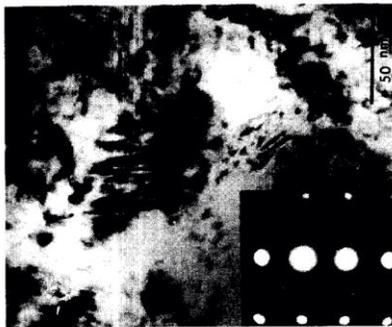


Figure 2.- TEM bright field image of Fe<sub>50</sub>Cu<sub>50</sub> mechanically alloyed and heated up to 623 K.

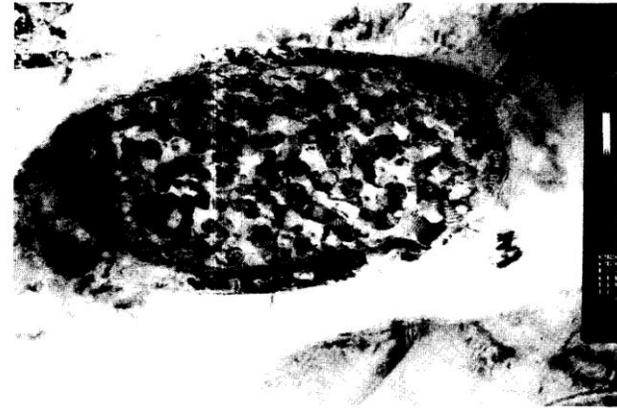


Figure 3.- TEM bright field image of melt-spun (Fe<sub>80</sub>Cu<sub>20</sub>)<sub>99</sub>B<sub>1</sub>.

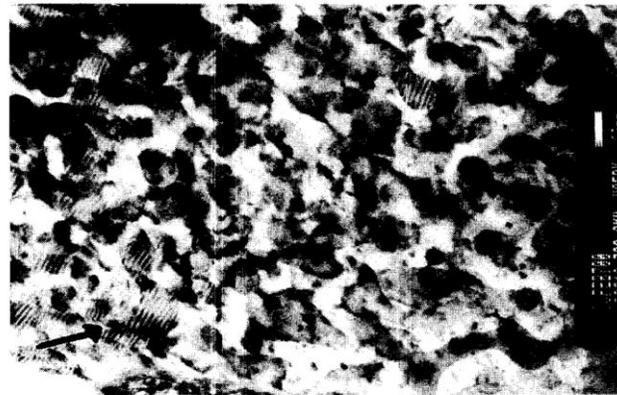


Figure 4.- TEM bright field image of melt-spun (Fe<sub>80</sub>Cu<sub>20</sub>)<sub>99</sub>B<sub>1</sub>.

#### 4. Conclusions.

In conclusion, TEM observations have shown the presence of contrast modulations in well defined crystallographic directions, with a modulating wavelength of few nanometers, which can be ascribed to spinodal decomposition in mechanically alloyed fcc Fe<sub>50</sub>Cu<sub>50</sub> as well as of fcc (Fe<sub>20</sub>Cu<sub>80</sub>)<sub>99</sub>B<sub>1</sub> liquid solutions.



## MÖSSBAUER SPECTROSCOPY EVIDENCE OF A SPINODAL MECHANISM FOR THE THERMAL DECOMPOSITION OF F.C.C. FeCu

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In summary, low and room temperature Mössbauer spectroscopy show that the decomposition process upon thermal treatment of metastable f.c.c. FeCu solid solution gives rise to composition

fluctuations, with different Fe environments. These fluctuations are evidence of the spinodal-like decomposition of the metastable FeCu solid solution.

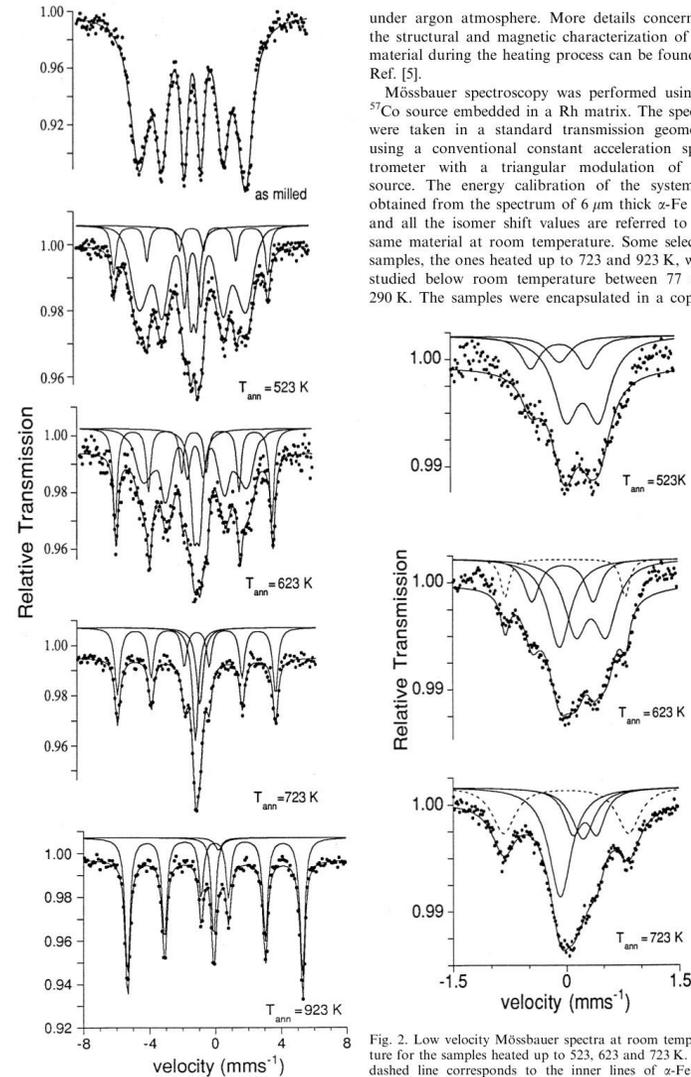


Fig. 1. Room temperature Mössbauer spectra for the as-milled and heated material.

under argon atmosphere. More details concerning the structural and magnetic characterization of the material during the heating process can be found in Ref. [5].

Mössbauer spectroscopy was performed using a <sup>57</sup>Co source embedded in a Rh matrix. The spectra were taken in a standard transmission geometry using a conventional constant acceleration spectrometer with a triangular modulation of the source. The energy calibration of the system is obtained from the spectrum of 6 μm thick α-Fe foil and all the isomer shift values are referred to the same material at room temperature. Some selected samples, the ones heated up to 723 and 923 K, were studied below room temperature between 77 and 290 K. The samples were encapsulated in a copper

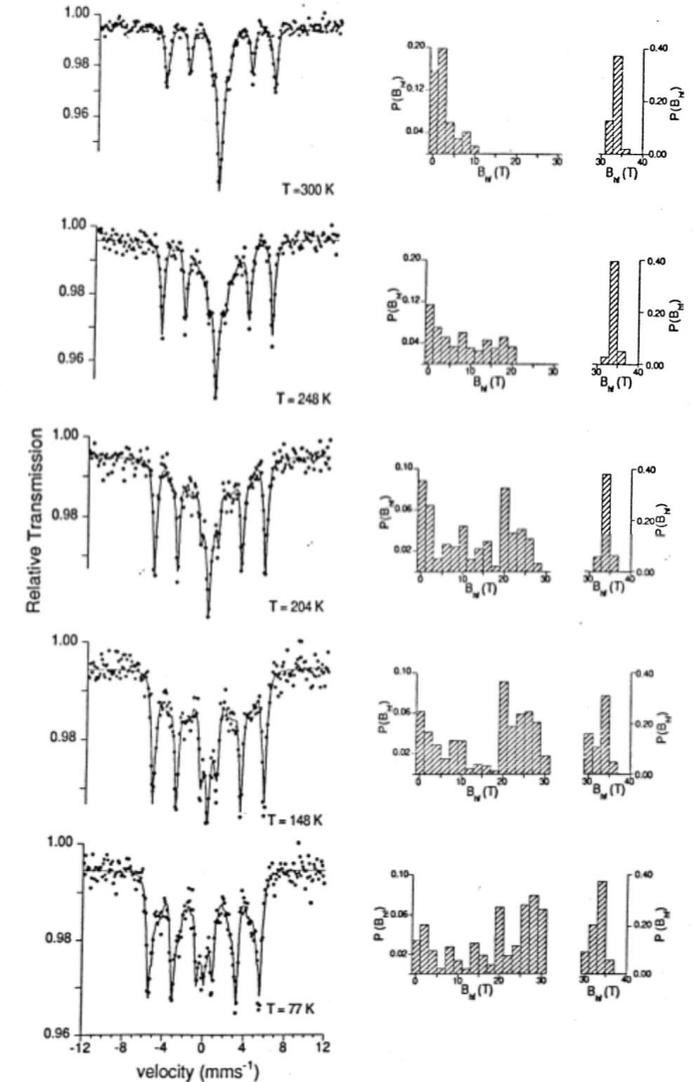


Fig. 3. Variable temperature Mössbauer spectra for the sample heated up to 723 K and the corresponding hyperfine distribution.

**Near-neighbor mixing and bond dilation in mechanically alloyed Cu-Fe**

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(Received 5 January 1996; revised manuscript received 4 April 1996)

Extended x-ray-absorption fine-structure (EXAFS) measurements were used to obtain element-specific, structural, and chemical information of the local environments around Cu and Fe atoms in high-energy ball-milled  $\text{Cu}_x\text{Fe}_{1-x}$  samples ( $x=0.50$  and  $0.70$ ). Analysis of the EXAFS data shows both Fe and Cu atoms reside in face-centered-cubic sites where the first coordination sphere consists of a mixture of Fe and Cu atoms in a ratio which reflects the as-prepared stoichiometry. The measured bond distances indicate a dilation in the bonds between unlike neighbors which accounts for the lattice expansion measured by x-ray diffraction. These results indicate that metastable alloys having a positive heat of mixing can be prepared via the high-energy ball-milling process. [S0163-1829(96)10033-3]



Dresden



Post-doc

## High remanence NdFeBX (X = Cu, Si, Nb<sub>3</sub> Cu, Zr) powders by mechanical alloying

V. Neu, P. Crespo, R. Schäfer, J. Eckert, L. Schultz

# Remanence enhancement in mechanically alloyed two-phase Nd-Fe-B magnetic material

**ARTICLE** in MATERIALS LETTERS 26(3):167-170 · FEBRUARY 1996 *with* 4 READS

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IF 29.04 · Chalmers University of Technology



3rd **R. Schäfer**



Last **L. Schultz**



***Fe***



***Cu***

## Materials Science and Engineering: A

15 June 1997, Vol.226:577–580, doi:10.1016/S0921-5093(97)80066-4

Ninth International Conference on Rapidly Quenched and Metastable Materials

Structural and magnetic properties of  
nanocrystalline  $(\text{Fe-Cu})_{93}\text{Zr}_7$  alloys prepared by  
mechanical alloying

C. Stiller, J. Eckert, P. Crespo, S. Roth, L. Schnitz



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## Magnetic and Mössbauer characterization of (Fe<sub>0.5</sub>Cu<sub>0.5</sub>)<sub>100-x</sub>Zr<sub>x</sub> alloys

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|                     |   |
|---------------------|---|
| <b>Autor</b>        | Multigner Domínguez, Marta María  |
| <b>Título</b>       | <b>Diseño, obtención y caracterización de nuevos materiales magnéticos : sistema FeCuZr : una aplicación en biomedicina / Marta M<sup>a</sup> Multigner Domínguez</b>   |
| <b>Publicación</b>  | 2004  |
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Pd

### Ferromagnetism in fcc Twinned 2.4 nm Size Pd Nanoparticles

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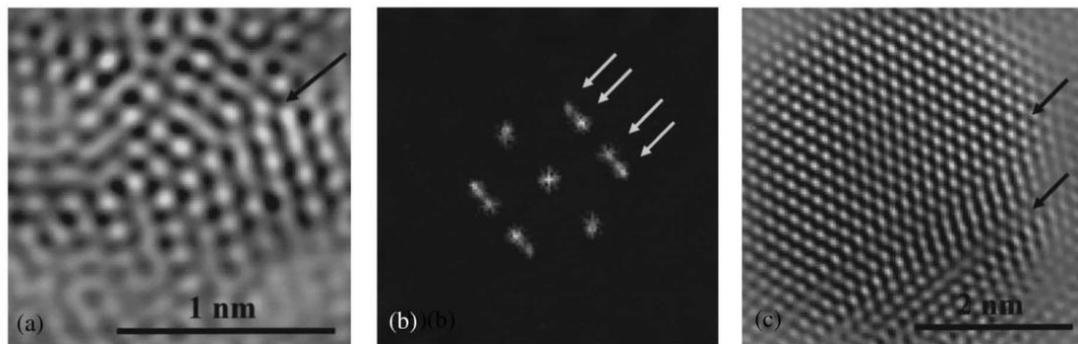


FIG. 2. (a) Fourier filtered HRTEM image of a Pd nanoparticle (diameter = 2 nm). The twin boundary is arrowed. (b) Corresponding FT diffraction pattern along the [111] direction. The splitting of the FT spots due to twinning is indicated. (c) Fourier filtered HRTEM image of a Pd nanocrystal (diameter = 4.4 nm) showing two twin boundaries.

Local deviation from cubic symmetry near the twin boundaries could also be invoked to account for the ferromagnetic behavior [5]. The strong surface energy anisotropy acts as the driving force for twinning in small Pd clusters. Therefore, the twinning boundary density is expected, and experimentally observed in this Letter and in a previous paper [6], to be noticeably enhanced in small clusters. Consequently, we suggest that the onset of ferromagnetism, experimentally observed and reported increase of  $N(E_F)$  promotes the induction of a spontaneous magnetic moment.

In conclusion, we have observed the onset of ferromagnetism in fcc twinned 2.4 nm Pd nanoparticles.

saturation as is probably due to the coexistence of blocked ferromagnetic entities with superparamagnetic particles and paramagnetic atoms.

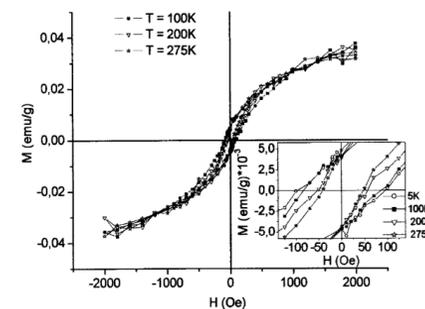


FIG. 3. Hysteresis loops at different temperatures of Pd nanoparticles. Inset: a more detailed view of the thermal coercivity response of the same sample.

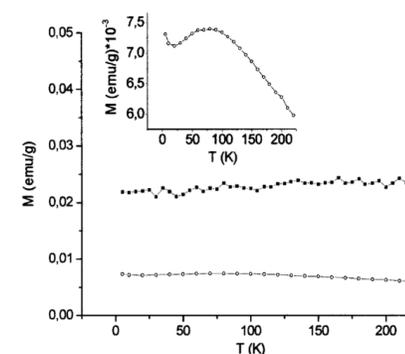


FIG. 4. Thermal dependence of magnetization under a dc applied field of 1 kOe for Pd 2.4 nm average mean particle size (solid squares) and bulk Pd (open circles). Inset: detailed thermal dependence for Pd bulk metal measured under the same applied field but plotted in a different scale.



# Fe + Rh

## Magnetic and magnetoelastic behavior of mechanically alloyed FeRh compound

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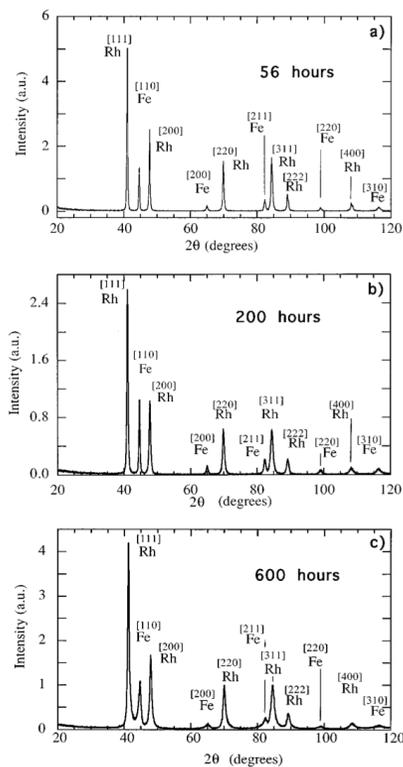


FIG. 2. X-ray diffraction patterns of the as milled sample, at different milling times, before annealing.

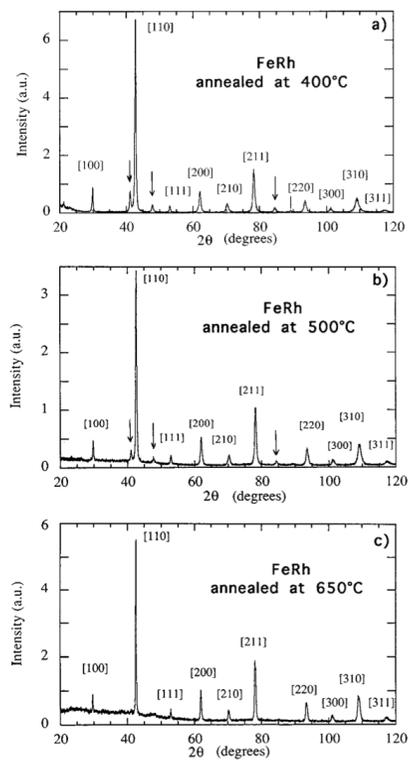


FIG. 3. Evolution of the mechanically alloyed FeRh crystal structure with the annealing temperature (arrows indicate spurious fcc peaks).

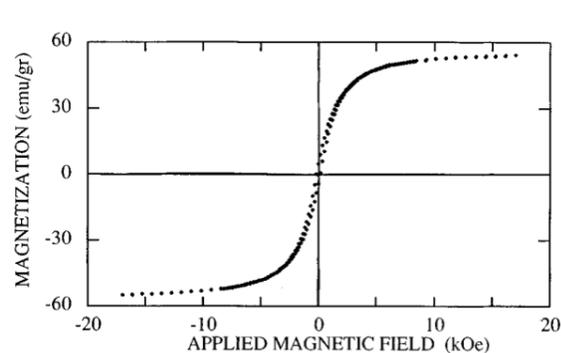


FIG. 6. Hysteresis loop of the 650 °C annealed sample, measured at room temperature.

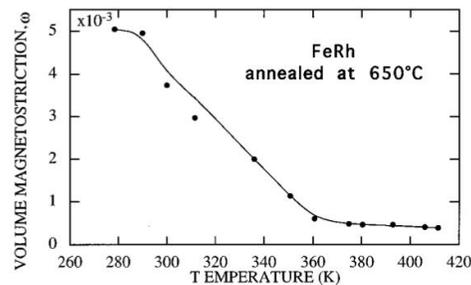


FIG. 7. Thermal dependence of the volume magnetostriction  $\omega$  at 14.2 T for mechanically alloyed FeRh, annealed at 650 °C.

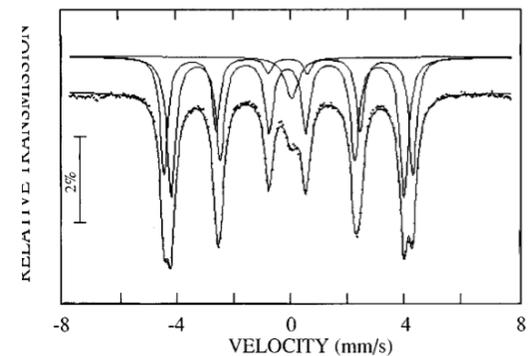


FIG. 5. Mössbauer spectrum of the the sample annealed at 650 °C measured at room temperature.

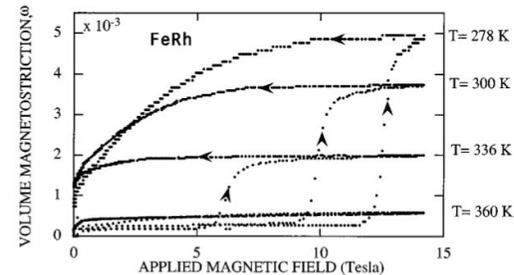


FIG. 8. Magnetostriction isotherms of mechanically alloyed FeRh, annealed at 650 °C.

## Permanent Magnetism, Magnetic Anisotropy, and Hysteresis of Thiol-Capped Gold Nanoparticles

350 citas

P. Crespo,<sup>1</sup> R. Litrán,<sup>2</sup> T. C. Rojas,<sup>2</sup> M. Multigner,<sup>1</sup> J. M. de la Fuente,<sup>3</sup> J. C. Sánchez-López,<sup>2</sup> M. A. García,<sup>1</sup> A. Hernando,<sup>1</sup> S. Penadés,<sup>3</sup> and A. Fernández<sup>2,\*</sup>

<sup>1</sup>*Instituto de Magnetismo Aplicado (RENFE-UCM-CSIC), P.O. Box 155, 28230 Las Rozas, Madrid, Spain and Departamento de Física de Materiales, Universidad Complutense, Madrid, Spain*

<sup>2</sup>*Instituto de Ciencia de Materiales de Sevilla CSIC-USE, Américo Vespucio nr.49, 41092 Sevilla, Spain and Departamento de Química Inorgánica, Universidad de Sevilla, Spain*

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(Received 13 March 2004; published 20 August 2004)

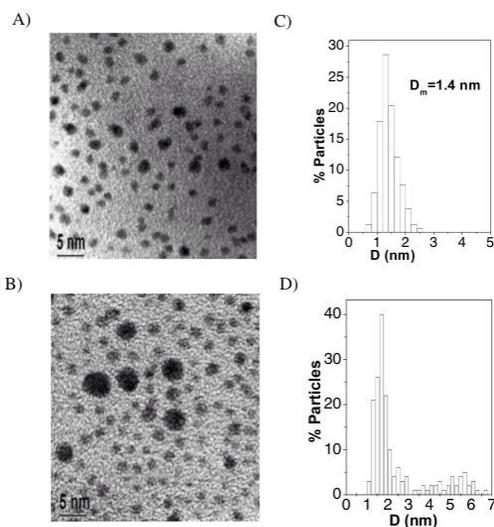


FIG. 1. Transmission electron micrographs of Au-SR (a) and Au-NR (b) NPs. Their corresponding histograms, obtained from several micrographs, are plotted, respectively, in (c) and (d).

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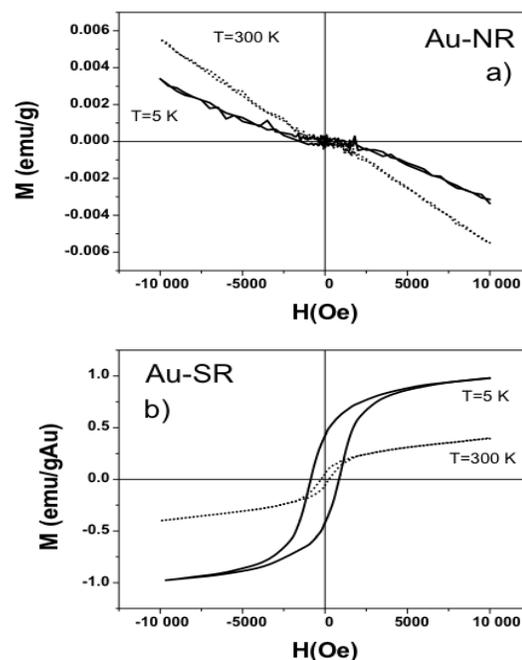


FIG. 3. Magnetization curves of gold nanoparticles stabilized by means of a surfactant, Au-NR (a), and hysteresis loops corresponding to the gold thiol-capped NPs, Au-SR (b), at 5 and 300 K. For the Au-SR sample, the magnetization is given in emu per gram of gold.

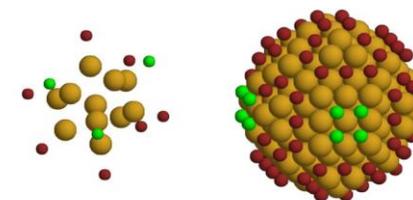


Fig. 2 Perspective view of the cluster and nanoparticle structure. On the left hand side panel, the subnanometric cluster  $Au_{11}$ -TPP with an icosahedral structure, whereas the fcc bulklike  $\sim 2$  nm Au-TPP nanoparticle is represented in the right hand side panel. The gold core atoms are yellow, the red balls correspond to phosphorus and the green ones to chlorine. For simplicity's sake, the aromatic rings of the triphenylphosphine molecule are not included.

**UNIVERSIDAD COMPLUTENSE DE MADRID**  
**FACULTAD DE CIENCIAS FÍSICAS**  
**DEPARTAMENTO DE FÍSICA DE MATERIALES**



**TESIS DOCTORAL**

**Nanoestructuras multifuncionales de Fe-Au y Fe-Pt**

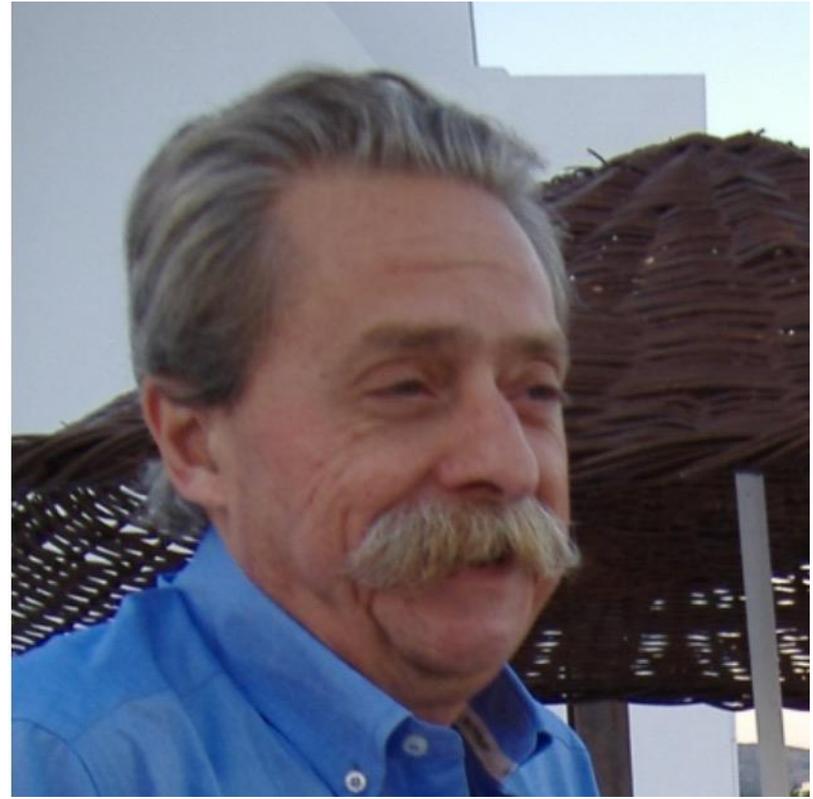
MEMORIA PARA OPTAR AL GRADO DE DOCTOR  
PRESENTADA POR

**Víctor Velasco Jimeno**

Directora

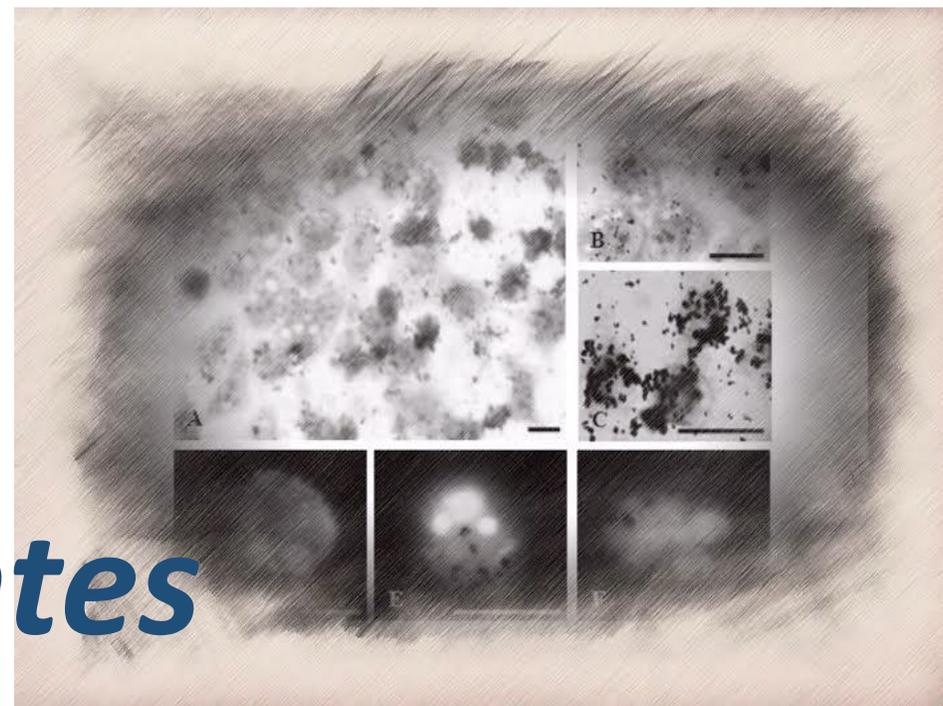
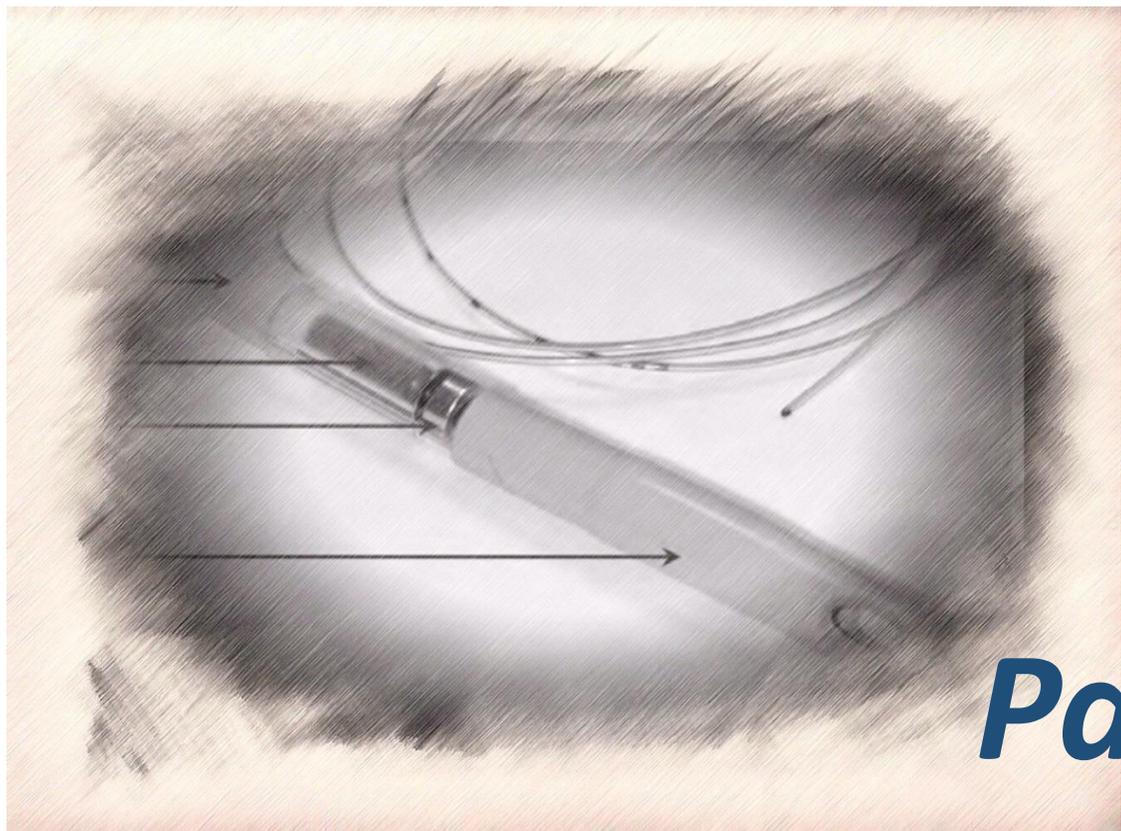
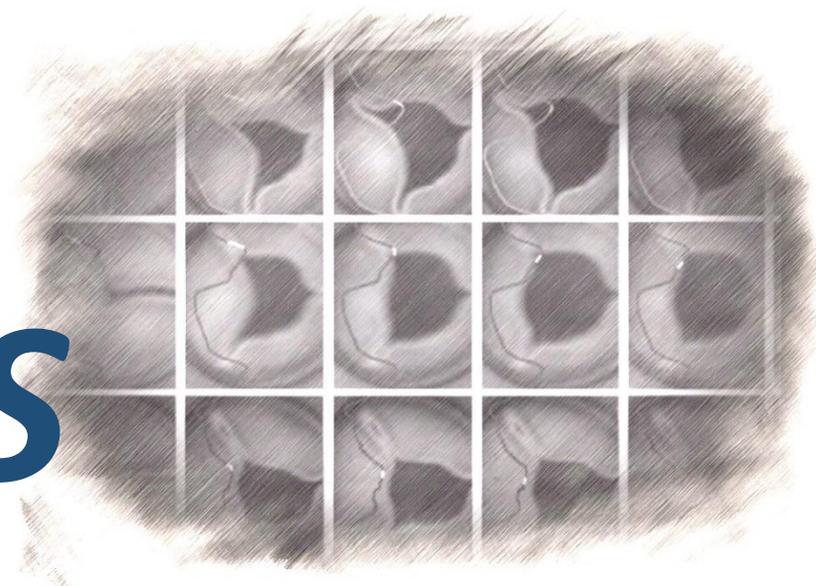
**Patricia Crespo del Arco**

**Madrid, 2015**

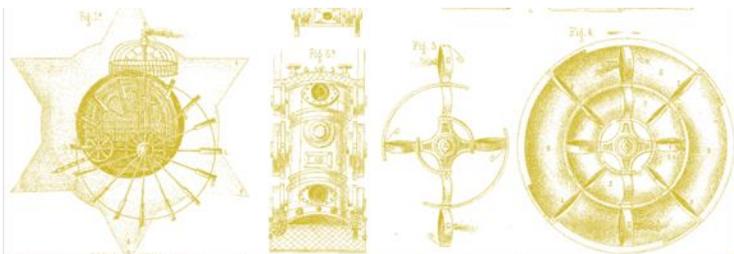


*Aplicaciones*

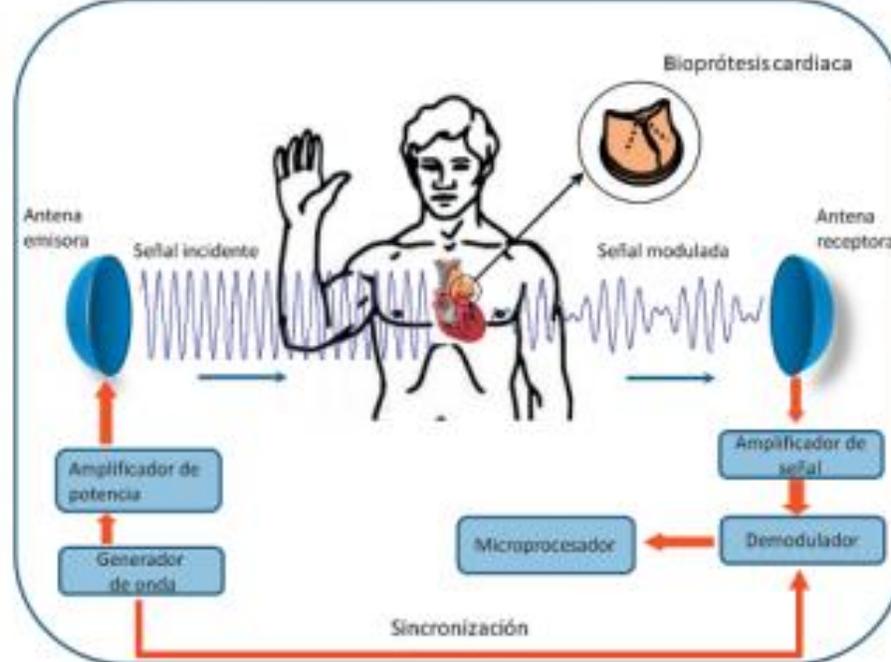
# *SENSORES*



*Patentes*



## 200 años de patentes



## Galería 9 El Futuro de la Propiedad Industrial

El ingenio del ser humano parece no tener límites. Los nuevos avances, entre otros, en biotecnología, robótica, nuevos materiales, comunicaciones o tecnologías de la información afectarán a aspectos fundamentales de nuestras vidas. Algunas de las patentes recientemente registradas nos ofrecen claves sobre EL FUTURO DE LA PROPIEDAD INDUSTRIAL.

### Tecnología médica

Las válvulas cardíacas biológicas, que a diferencia de las mecánicas no requieren mantenimiento ni tratamiento de anticoagulación, presentan sin embargo el inconveniente de una menor durabilidad y una mayor incertidumbre en su vida operativa. La invención patentada (ES 2312256) consiste en un sensor magnético que permite monitorizar el funcionamiento de estas prótesis cardíacas biológicas tras su implantación en pacientes. La utilización de este sensor evita riesgos al enfermo, ya que permite establecer con precisión el momento adecuado para la sustitución de la bioprótesis.

La invención, patentada por un grupo de investigación de la Universidad Complutense de Madrid en 2006, se basa en la im-

Imagen por gentileza de la Universidad Complutense de Madrid

corporación de un material magnético en cada uno de los velos valvulares de la prótesis. Durante la monitorización, se hace incidir sobre la bioprótesis una onda electromagnética a una frecuencia determinada. La onda incidente es absorbida en parte por el material magnético de los velos y transmitida hacia un receptor externo al paciente. El movimiento de los velos modula la señal transmitida. Las disfunciones producidas durante el proceso de apertura y cierre de la válvula de prótesis cardíaca provocan un cambio en la señal de funcionamiento óptimo, lo que permitiría a los servicios médicos establecer con precisión el momento en el que la válvula debe ser sustituida.

En el dibujo puede verse un esquema de funcionamiento del sensor.

# 23 patentes

**1. DIFFERENTIAL CALORIMETER AND METHOD FOR MEASURING THE SPECIFIC ABSORPTION RATE OF MAGNETIC COLLOIDS SUBJECTED TO ELECTROMAGNETIC FIELDS**

| Inventor:   | Applicant:                      | CPC:  | IPC:                               | Publication info:               | Priority date: |
|---|---------------------------------|---|------------------------------------|---------------------------------|----------------|
| RIVERO<br>RODRIGUEZ<br>GUILLERMO [ES]<br>MULTIGNER<br>DOMINGUEZ<br>MARTA [ES]<br>(+4) | UNIV MADRID COMPLUTENSE<br>[ES] | A61N1/40<br>G01K17/04<br>G01N25/486<br>A61N1/40 | G01K17/04<br>G01N25/48<br>A61N1/40 | WO2014181006 (A1)<br>2014-11-13 | 2013-05-10     |

**2. SISTEMA DE MEDIDA DE DEFORMACIONES DE RAILES FERROVIARIOS**

| Inventor:  | Applicant:   | CPC:                                       | IPC:                                     | Publication info:  | Priority date: |
|--|--|--|--|--|----------------|
| RIVERO<br>RODRIGUEZ<br>GUILLERMO [ES]<br>VALDES TAMAMES<br>JAVIER [ES]<br>(+5) | ADMINISTRADOR DE<br>INFRAESTRUCTURAS<br>FERROVIARIAS ADIF [ES] | B61K9/10<br>B61L23/047<br>G01B5/30<br>(+1) | G01B5/30<br>G01N3/20<br>B61K9/10<br>(+1) | ES2391333 (A1)<br>2012-11-23<br>ES2391333 (B1)<br>2013-10-02 | 2010-12-27     |

**3. DISPOSITIVO Y PROCEDIMIENTO PARA DETERMINAR EL TIEMPO DE COAGULACION DE SANGRE BASADO EN MAGNETOELASTICIDAD.**

| Inventor:  | Applicant:            | CPC:                     | IPC:                   | Publication info:  | Priority date: |
|--|-----------------------|--------------------------|------------------------|--|----------------|
| HERNANDO<br>GRANDE ANTONIO<br>[ES]<br>FLORES VIDAL<br>MARIA DE LA<br>SIERRA [ES]<br>(+6) | MICROMAG 2000 SL [ES] | G01N27/76<br>G01N33/4905 | G01N27/76<br>G01N33/49 | ES2373900 (A1)<br>2012-02-10<br>ES2373900 (B1)<br>2012-12-05 | 2010-07-06     |

**4. DISPOSITIVO PARA LA MEDIDA DE LA EVOLUCION DE LA MASA DE UN CULTIVO CELULAR "IN SITU" BASADO EN UN SENSOR MAGNETOELASTICO.**

| Inventor:  | Applicant:                      | CPC:                    | IPC:     | Publication info:  | Priority date: |
|--|---------------------------------|-------------------------|----------|--|----------------|
| CRESPO DEL ARCO<br>PATRICIA<br>PRESA MUNOZ DE<br>TORO PATRICIA<br>MARCEL<br>(+7) | UNIV MADRID COMPLUTENSE<br>[ES] | C12M1/3407<br>C12M41/36 | C12M1/34 | ES2352482 (A1)<br>2011-02-21<br>ES2352482 (B1)<br>2011-12-30 | 2008-07-01     |

**5. ESFINTER ARTIFICIAL INTRAURETRAL DE ACCIONAMIENTO MAGNETICO PARA PACIENTES FEMENINAS**

| Inventor:   | Applicant:    | CPC: | IPC:                  | Publication info:           | Priority date: |
|---|---------------|------|-----------------------|-----------------------------|----------------|
| RIVERO<br>RODRIGUEZ<br>GUILLERMO [ES]<br>MULTIGNER<br>DOMINGUEZ MA<br>MARTA<br>(+3) | INDAS S A LAB |      | (IPC1-7):<br>A61F2/48 | AR041819 (A1)<br>2005-06-01 | 2003-10-22     |

**6. LOW-CONSUMPTION MAGNETIC-FIELD SENSOR**

| Inventor:   | Applicant:            | CPC:   | IPC:                               | Publication info:  | Priority date: |
|---|-----------------------|--|------------------------------------|--|----------------|
| RIVERO<br>RODRIGUEZ<br>GUILLERMO [ES]<br>MARIN PALACIOS<br>PILAR [ES]<br>(+3) | MICROMAG 2000 SL [ES] | G01R33/02<br>G01R33/063<br>G01R33/18<br>(+2) | G01R33/02<br>H01B1/02<br>H01F1/153 | ES2333575 (A1)<br>2010-02-23<br>ES2333575 (B1)<br>2010-11-26 | 2008-06-30     |

**8. SENSOR MAGNETICO DE DETECCION DEL DETERIORO DE PROTESIS CARDIACAS Y METODO DE DETECCION.**

| Inventor:   | Applicant:                      | CPC:                     | IPC:                  | Publication info:  | Priority date: |
|---|---------------------------------|--------------------------|-----------------------|--|----------------|
| RIVERO<br>RODRIGUEZ<br>GUILLERMO [ES]<br>MULTIGNER<br>DOMINGUEZ MARTA<br>MARIA [ES]<br>(+4) | UNIV MADRID COMPLUTENSE<br>[ES] | A61B5/0002<br>A61F2/2472 | A61F2/24<br>A61B5/024 | ES2312256 (A1)<br>2009-02-16<br>ES2312256 (B1)<br>2009-12-22 | 2006-06-30     |

**9. External magnetic actuation valve for intraurethral artificial urinary sphincter**

| Inventor:   | Applicant:                      | CPC:       | IPC:  | Publication info:            | Priority date: |
|---|---------------------------------|------------|---|------------------------------|----------------|
| RIVERO<br>RODRIGUEZ<br>GUILLERMO [ES]<br>MULTIGNER<br>DOMINGUEZ<br>MARTA [ES]<br>(+4) | UNIV MADRID COMPLUTENSE<br>[ES] | A61F2/0018 | A61F2/00<br>A61F2/04<br>(IPC1-7):<br>A61F2/00 | US6623421 (B1)<br>2003-09-23 | 1999-02-11     |

**10. Current system for compensating the magnetic field produced by electric traction railways**

| Inventor:   | Applicant:                      | CPC:     | IPC:                                      | Publication info:            | Priority date: |
|---|---------------------------------|----------|---|------------------------------|----------------|
| HERNANDO<br>GRANDE ANTONIO<br>[ES]<br>RIVERO<br>RODRIGUEZ<br>GUILLERMO [ES]<br>(+2) | UNIV MADRID COMPLUTENSE<br>[ES] | B60M1/06 | B60M1/06<br>B61B13/00<br>H02G1/02<br>(+1) | US6492746 (B1)<br>2002-12-10 | 1999-02-04     |

**11. Miniature magnetic field sensor e.g. fluxgate, has small, ferromagnetic and helical magnetic core, which measures magnitude and direction of magnetic fields or continuous alternating fields of low frequency**

| Inventor:   | Applicant:                      | CPC:      | IPC:      | Publication info:  | Priority date: |
|---|---------------------------------|-----------|-----------|--|----------------|
| RIVERO<br>RODRIGUEZ<br>GUILLERMO [ES]<br>HERNANDO<br>GRANDE ANTONIO<br>[ES]<br>(+3) | UNIV MADRID COMPLUTENSE<br>[ES] | G01R33/04 | G01R33/04 | ES2281253 (A1)<br>2007-09-16<br>ES2281253 (B2)<br>2008-03-16 | 2005-07-28     |

**12. Measuring device for direct measurement of magnetostriction volume of magnetic materials, comprises container holder with tight closing except for capillary section, where holder is filled with liquid**

| Inventor:   | Applicant:                      | CPC:      | IPC:      | Publication info:  | Priority date: |
|---|---------------------------------|-----------|-----------|--|----------------|
| RIVERO<br>RODRIGUEZ<br>GUILLERMO [ES]<br>MULTIGNER<br>RODRIGUEZ<br>MARTA [ES]<br>(+1) | UNIV MADRID COMPLUTENSE<br>[ES] | G01R33/18 | G01R33/18 | ES2278482 (A1)<br>2007-08-01<br>ES2278482 (B1)<br>2008-06-16 | 2004-11-26     |

**13. MAGNETICALLY-ACTUATED ARTIFICIAL INTRAURETHRAL SPHINCTER FOR FEMALE PATIENTS**

| Inventor:   | Applicant:         | CPC:                       | IPC:                              | Publication info:  | Priority date: |
|---|--------------------|----------------------------|-----------------------------------|--|----------------|
| RIVERO<br>RODRIGUEZ<br>GUILLERMO [ES]<br>MULTIGNER<br>DOMINGUEZ MARTA<br>M [ES]<br>(+4) | INDAS S A LAB [ES] | A61F2/0022<br>A61F2210/009 | A61F2/48<br>(IPC1-7):<br>A61F2/48 | ES2214117 (A1)<br>2004-09-01<br>ES2214117 (B1)<br>2006-02-16 | 2002-10-22     |

# Magnetic Sensors for Biomedical Applications

CHAPTER · MARCH 2012

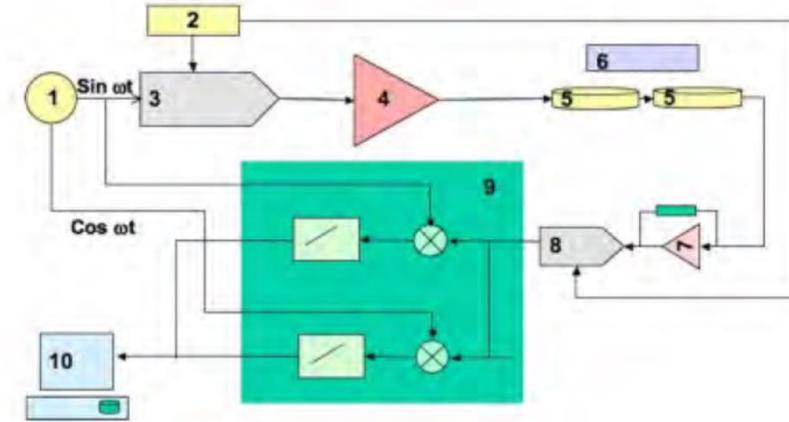
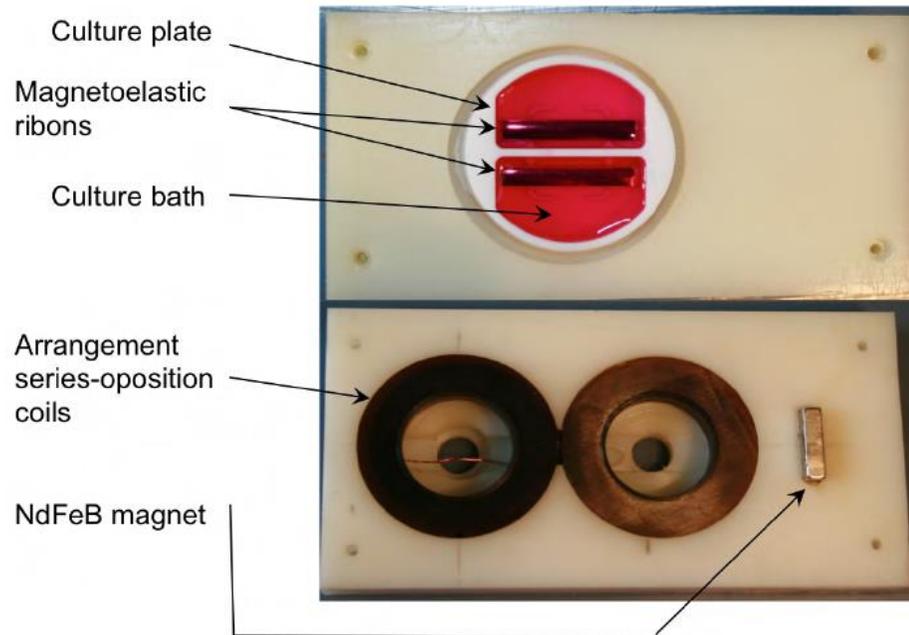
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**7**

## **Magnetic Sensors for Biomedical Applications**

Guillermo Rivero, Marta Multigner and Jorge Spottorno  
*Instituto de Magnetismo Aplicado (Universidad Complutense de Madrid)*  
*Spain*

## 2.1 *In situ* measurement of the mass evolution of cell culture



1) Direct Digital Synthesizer; 2) Voltage reference; 3) D/A Converter; 4) Power amplifier; 5) Exciting/Pick up coils; 6) Magnetoelastic sensor; 7) Voltage/Current Converter; 8) A/D converter; 9) Digital signal processor; 10) Acquisition

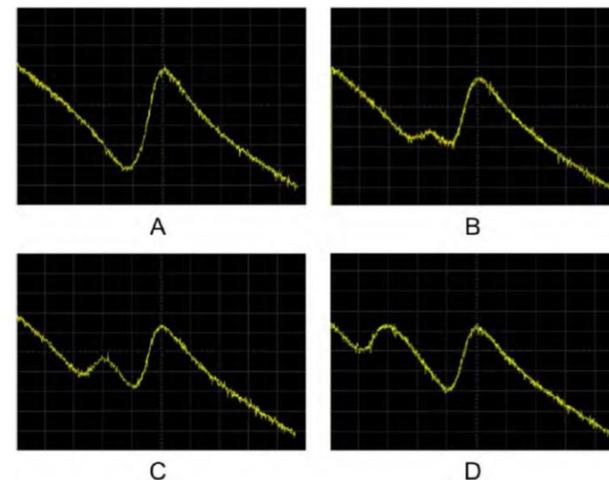


Fig. 3. Evolution of the resonance of ribbons arrangement. In the initial state A, both ribbons have the same resonance frequency. The left peak increases and decreases its frequency with the amount of mass on the corresponding ribbon.

## 2.2 Test of blood coagulation

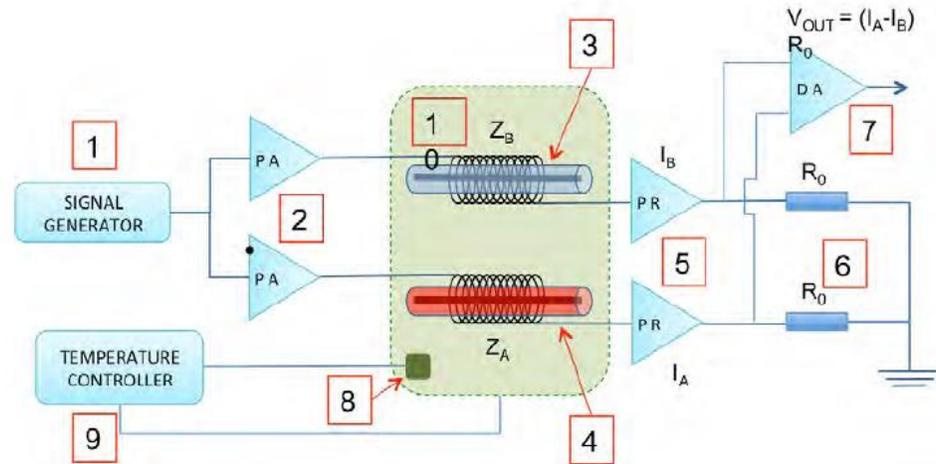


Fig. 4. Scheme of the experimental setup used to measure the blood coagulation.

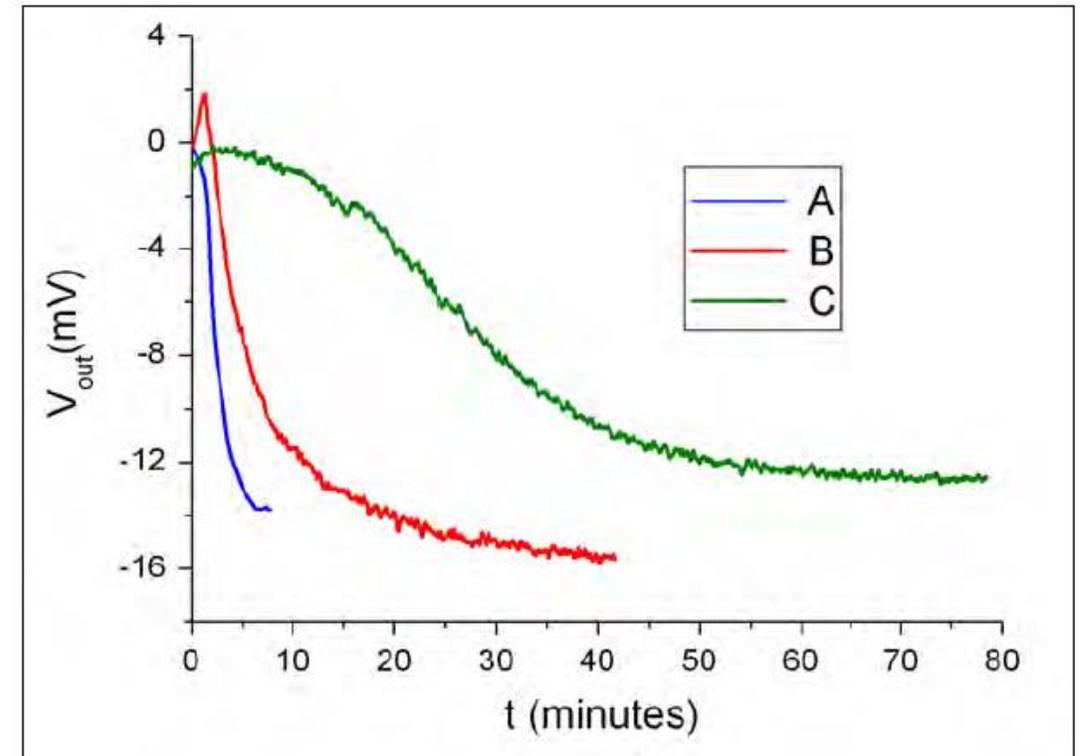


Fig. 5. Study of the influence in the coagulation of blood with different amounts of coagulant agent. The amount of blood is 200  $\mu$ l, and was mixed with 5  $\mu$ l of coagulant (curve A), 1  $\mu$ l of coagulant (curve B), and without coagulant (curve C).

## 2.3 Sensor system for early detection of heart valve bioprostheses failure

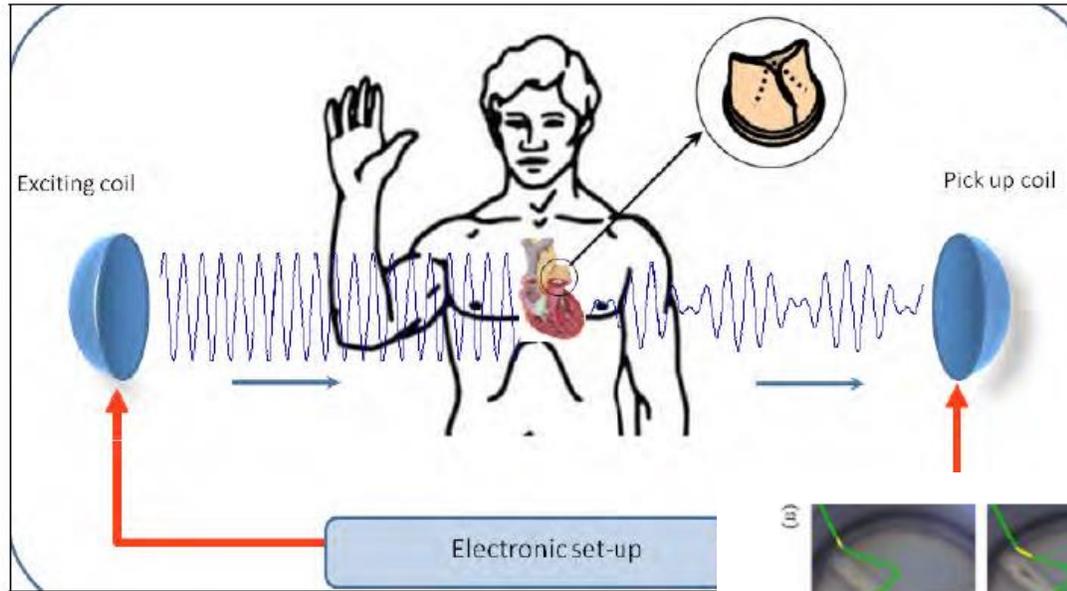


Fig. 7. Detection of motion of bioprostheses cusps with micro

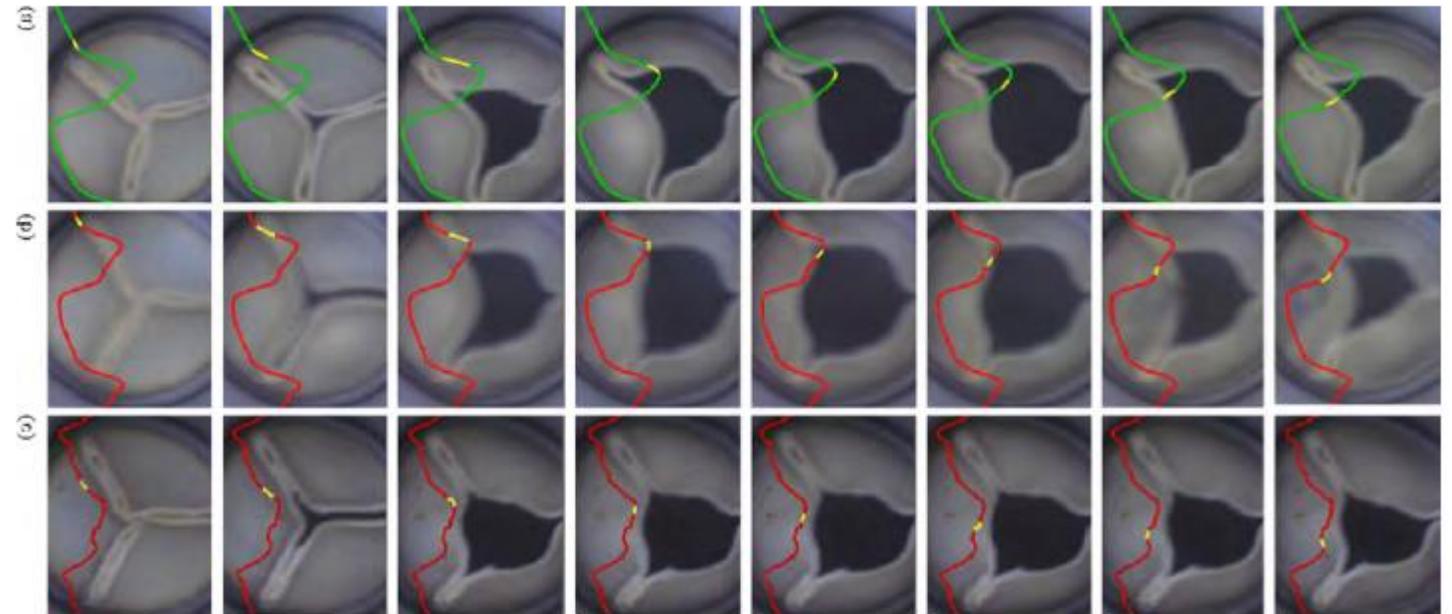


Fig. 8. Opening process of the valve with different damage levels.

### 3.1 Magnetic endoluminal artificial urinary sphincter

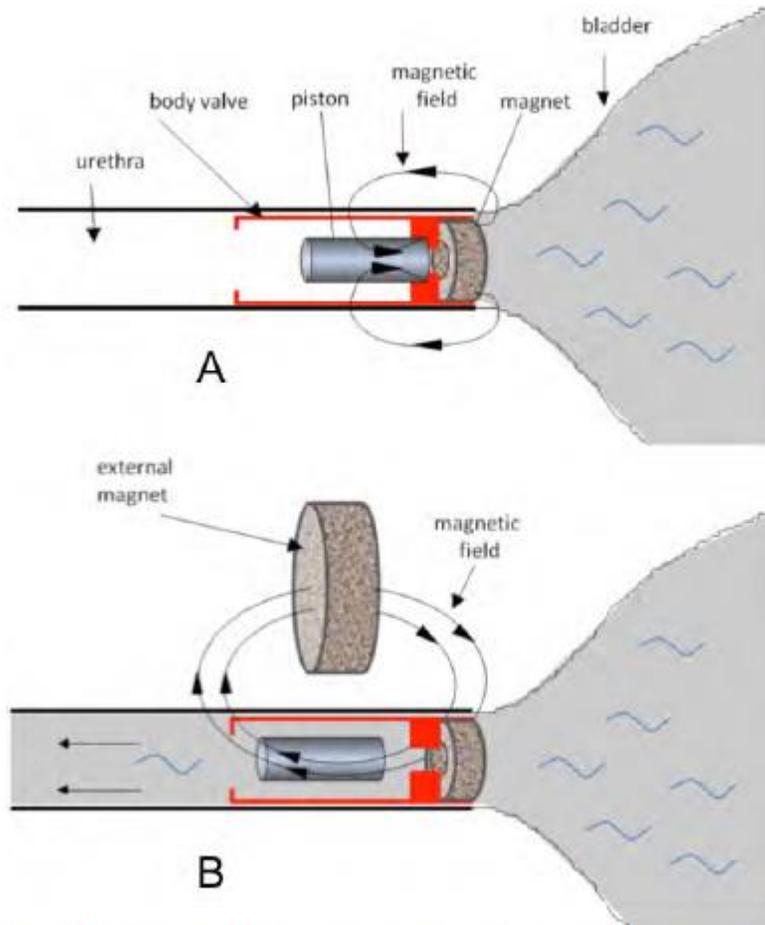


Fig. 11. Sketch of the magnetic valve operation. A) Closed position. B) Open position.

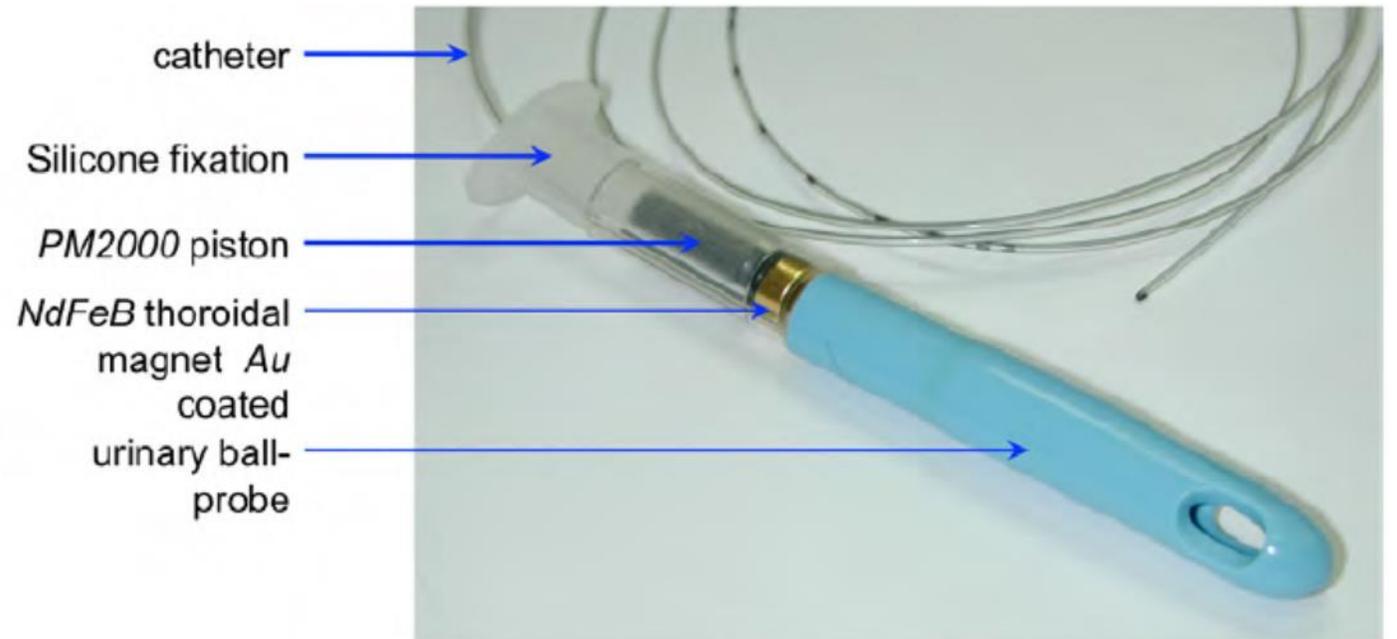


Fig. 10. Sphincter prototype for trials on animal models.

## 3.2 Hyperthermia HeLa cell treatment with silica-coated manganese oxide nanoparticles

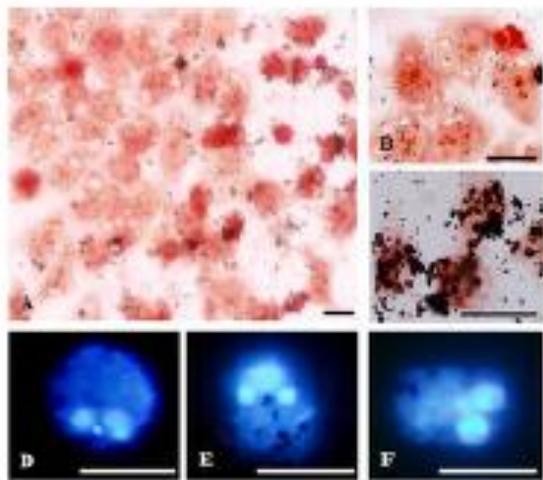


Fig. 12. Nanoparticles (black spots) inside the cell after apoptosis (White holes) (Villanueva, 2010)

### Study of Heating Efficiency as a Function of Concentration, Size, and Applied Field in $\gamma$ -Fe<sub>2</sub>O<sub>3</sub> Nanoparticles

P. de la Presa,<sup>\*,†,‡</sup> Y. Luengo,<sup>§</sup> M. Multigner,<sup>†</sup> R. Costo,<sup>§,⊥</sup> M. P. Morales,<sup>§</sup> G. Rivero,<sup>†,‡</sup> and A. Hernando<sup>†,‡</sup>

<sup>†</sup>Instituto de Magnetismo Aplicado (UCM-ADIF-CSIC), P.O. Box 155, Las Rozas, Madrid 28230, Spain

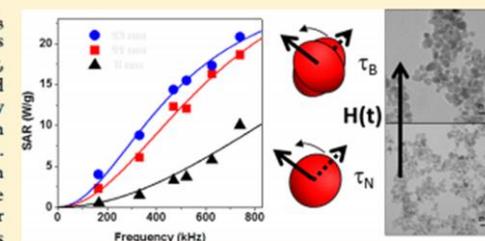
<sup>‡</sup>Departamento de Física de Materiales, Universidad Complutense de Madrid, Madrid, Spain

<sup>§</sup>Departamento de Biomateriales y Materiales Bioinspirados, Instituto de Ciencia de Materiales de Madrid/CSIC, Sor Juana Inés de la Cruz 3, Campus de Cantoblanco, Madrid 28049, Spain

<sup>⊥</sup>Van't Hoff Laboratory for Physical and Colloid Chemistry, Utrecht University, Padualaan 8, 3584 CH Utrecht, Netherlands

#### Supporting Information

**ABSTRACT:** The specific absorption rate (SAR) of  $\gamma$ -Fe<sub>2</sub>O<sub>3</sub> nanoparticles (NPs) under an alternating magnetic field has been investigated as a function of size, concentration, coating, liquid carrier, and frequency and amplitude of the applied magnetic field. The NPs have been synthesized by coprecipitation method with sizes ranging from 6 to 14 nm with low polydispersity (0.2) and high crystallinity degrees. The small NPs size (6–14 nm) and the value of the maximum applied field (<7.5 kA/m) allow the use of the linear response theory for the analysis of the experimental SARs values. Under this condition, Neel–Brown relaxation times of about 10<sup>-7</sup> s are obtained from SAR field frequency dependence. The NPs have been immobilized in agar to investigate the heating mechanisms, i.e., inversion of the magnetic moments inside the monodomain volume or particle rotation. The results suggest that there is a critical size of around 12 nm for obtaining the most effective heating in viscous media. Furthermore, the surface modification by aminopropylsilane coating does not affect the heating efficiency, making these NPs good candidates for hyperthermia treatment as well as model samples for standardization of hyperthermia apparatus.



## In Vivo Measurements of Electrical Conductivity of Porcine Organs at Low Frequency: New Method of Measurement

J. Spottorno,<sup>1,2\*</sup> M. Multigner,<sup>1,2</sup> G. Rivero,<sup>1,2</sup> L. Álvarez,<sup>3</sup> J. de la Venta,<sup>1,2</sup> and M. Santos<sup>3</sup>

<sup>1</sup>Institute of Applied Magnetism, Madrid, Spain

<sup>2</sup>Department of Materials Physics, Complutense University of Madrid, Madrid, Spain

<sup>3</sup>University Hospital Puerta de Hierro, Madrid, Spain

614 Spottorno et al.

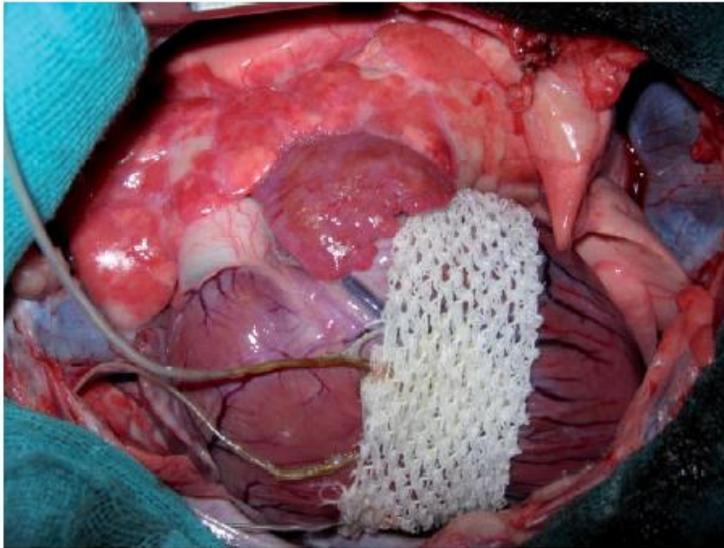


Fig. 1. Fixation of the platinum electrodes on a heart for the in vivo measurements.

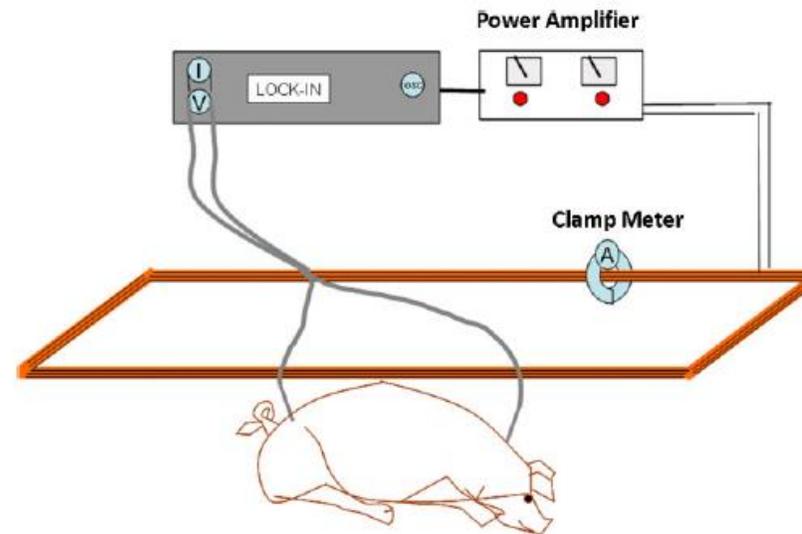


Fig. 2. Experimental setup for the in vivo measurements.



Fig. 3. Image of the measurements performed in the operating room.

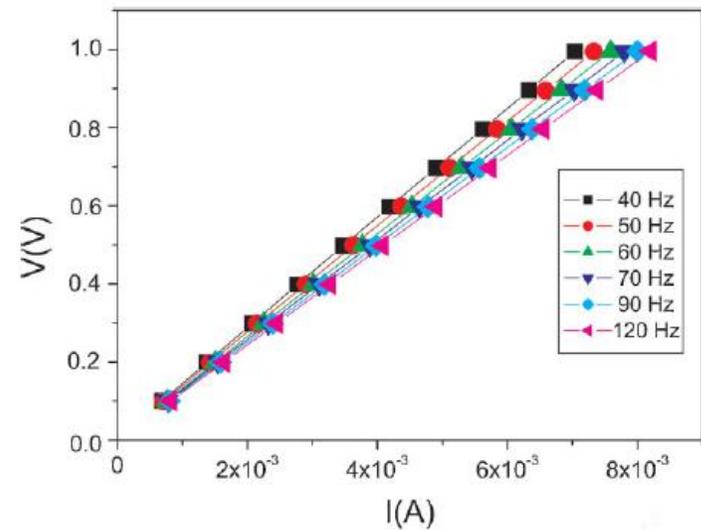


Fig. 4. Example of an I-V curve for several frequencies measured in a liver in vivo with platinum electrodes in two-electrode mode.

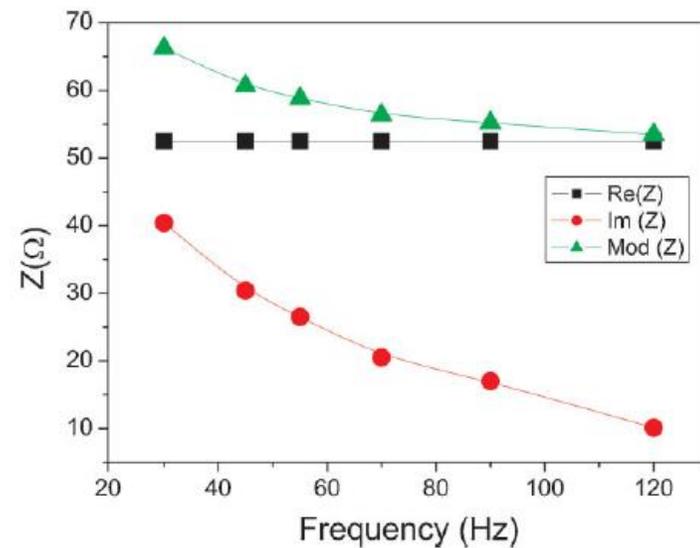


Fig. 5. Impedance of a kidney and its real and imaginary components measured with the induced voltage difference method and gold electrodes.



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B61L 23/04 (2006.01)

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Titular/es:

ADMINISTRADOR DE INFRAESTRUCTURAS  
FERROVIARIAS (ADIF) (100.0%)  
TITAN N<sup>os</sup> 4 y 6  
28045 MADRID (Madrid) ES

Inventor/es:

RIVERO RODRIGUEZ, Guillermo;  
VALDÉS TAMAMES, Javier;  
SPOTTORNO GINER, Jorge;  
MULTIGNER DOMINGUEZ, Marta Maria;  
FLORES VIDAL, Maria De La Sierra;  
HERNANDO GRANDE, Antonio y  
RODRIGUEZ PLAZA, Miguel

Agente/Representante:

UNGRÍA LÓPEZ, Javier

## 64 Título: SISTEMA DE MEDIDA DE DEFORMACIONES DE RAÍLES FERROVIARIOS

### 67 Resumen:

Sistema de medida de deformaciones de raíles ferroviarios.

Comprende uno o más sensores (1) que se fijan al rail (3) y se caracteriza porque el sensor comprende: una célula de carga (7, 8) que genera una señal proporcional al radio de curvatura que se produce en el rail (3) cuando se deforma por flexión; un acelerómetro de tres ejes (20) para medir las cargas dinámicas soportadas por el rail (3) al paso del tren, que además realiza funciones de inclinómetro de dos ejes para medir la inclinación del rail (3) tanto en sentido longitudinal como en el transversal; y un procesador de obtención de la medida de los parámetros para determinar la deformación del rail (3). Comprende medios de comunicación inalámbrica para comunicar con otros sensores y/o con un centro de procesado y establecer la evolución de la deformación de un tramo de rail (3).

La fijación al rail se realiza mediante imanes (9) que facilitan su montaje/desmontaje.

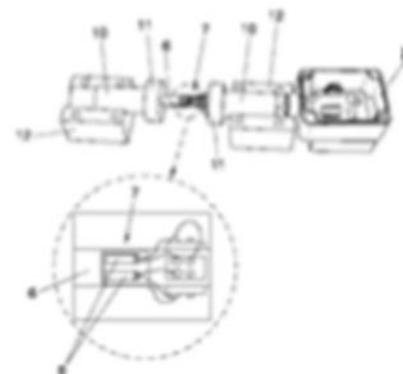
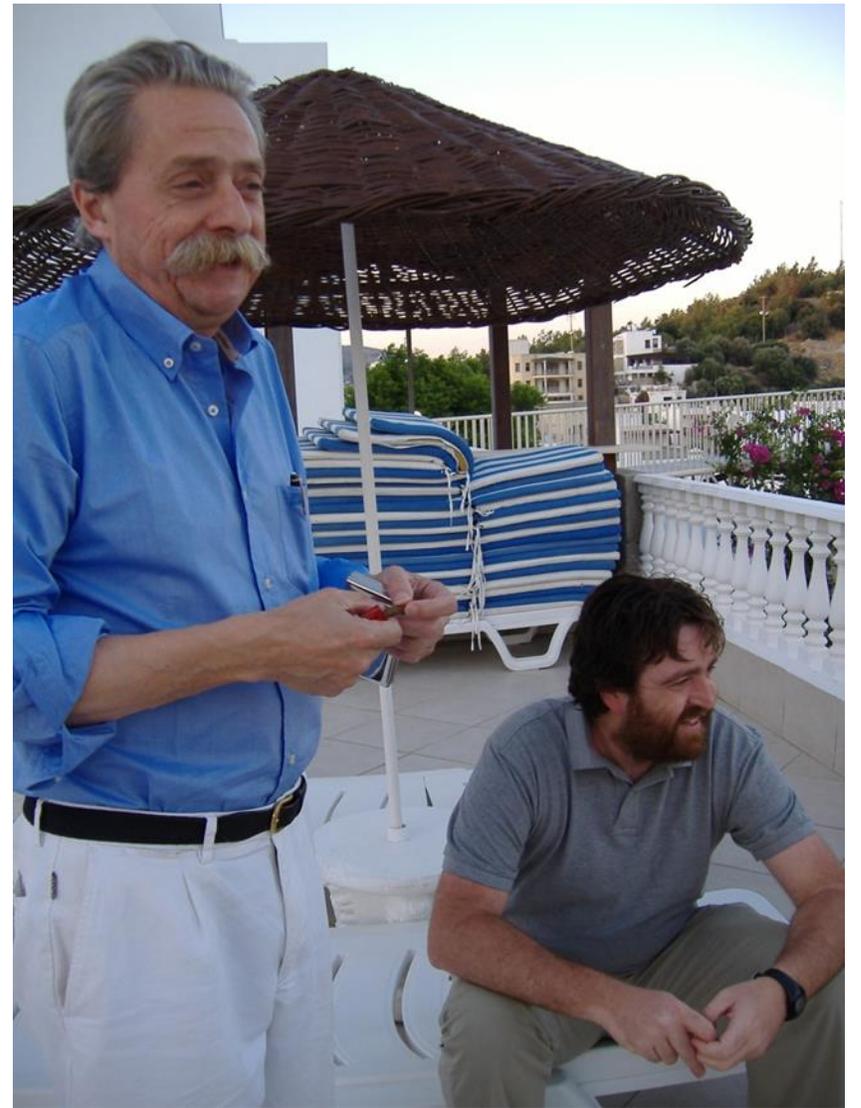


FIG. 3

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**GRACIAS**